

A Survey on Welding Characteristics of Submerged Arc Welding (SAW) on Mild Steel

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Abstract:

A welding process in which the molten weld and arc zone are protected from air pollution under fusible flux is called submerged arc welding (SAW). The process is usually limited to a horizontal fillet-fillet, but with a high degree of placement. These processes are combined with molten metal and when this molten metal's combine with the atmosphere to form oxides and nitrides. All arc welding processes use specific methods to protect the molten welding dam. The Submerged Arc Welding process is generally popular because it provides high production quality, high melting efficiency, easy automatic efficiency and low user requirement. For the purpose of obtaining a composite combination with the desired parameters for weld-bead, excellent mechanical properties with minimal distortion generally, all welding processes are used. Due to its ease of use, high current density and the ability to insert a large amount of welding metal using more than one wire at a time the Submerged Arc Welding (SAW) process is a major industrial application. Welding quality depends on the geometry of the weld beads also depends on the flexibility of the process. A very important role in determining the quality of the weld joint played by the Welding installation parameters. In terms of structures such as weld-bead geometry, mechanical properties, and distortion the joint quality can be assessed.

Keywords- Joint, Welding parameters, Flux, Submerged Arc Welding (SAW)

I. INTRODUCTION

Summerged arc welding (SAW) is a welding process in which the molten weld and arc zone are protected from air pollution under fusible flux. The process is usually limited to horizontal welding-fillet, but with a higher set-up, even where we use a continuous wire electrode. Submerged arc welding (SAW) is widely used to heat dense plates with high levels of metal inserts. The heat of this process is found in the arc between the stainless steel electrode and the work. SAW is different from other arc welding processes because the arc is not visible. It is protected by the coating of a composite granular substance called flux, which is deposited in the joint area before the arc. Pressure is not applied, and the filling metal is found mainly in the empty electrode wire provided continuously with arc flow coil and molten flow dam. A unique feature of SAW is that the granular flux material closes the welding area and prevents the emission of

arc rays, sparks, particles, and smoke. In addition to protecting the arc from viewing, the flux produces slag that protects the welding metal, reduces the cooling rate and helps shape the weld contour. Submerged arc welding (SAW) is probably the most widely used method of welding the web bridge so that the flange fillet weld and inline butt burn with a thick plate forming the flange and the length of the web. A continuous cable that uses a contact tip forms a molten pool. The weld pool is immersed in a flux fed form.

II. PRINCIPLE OF GMAW

The welding process in which a metal electrode is used to produce an electric arc to bind pieces of metal together in a protective gas field is called MIG (Metal Inert Gas) Or Gas Metal Arc Welding (GMAW). Gas protection protects the weld from air pollution. A continuous voltage, a direct current source of energy is used to produce an arc.

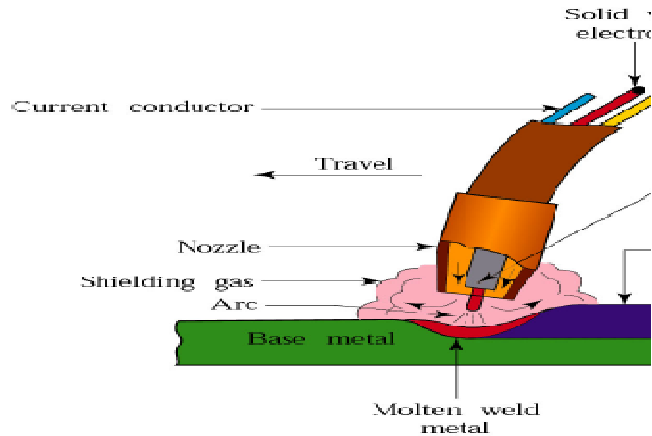


Fig No. 1.1(GMAW)

This welding was initiated in 1940 to melt aluminum and other non-metallic materials. This process can be semi-automatic or automatic. As a protective gas because these two are very rich and inert, it uses argon and helium. Metal heat transfer to MIG is done in four main modes and these are short-circuiting, spray, and pulsed-spray. Each of the method has its own limitations, personality, benefits and related characteristics

III. LITERATURE SURVEY

From time immemorial, the GMAW was designed for a large proportion of a combination of steel and effective anti-kiljoysteel. The effect of heat treatment for example pre-heating temperatures, between extreme temperatures, post-heating temperatures (PWHT) has also been evaluated. Many analytical models were developed using limited analysis, as well as a neural network. A summary of the work done before that on GMAW is applicable at this stage.

IV. BRIEF LITERATURE SURVEY

Overall, GMAW services in Cr-mo steel have been successful; there is still much work to be done. The work done on the topic is described below:

W. Provost (1982) examined the effects of warm behavior on reducing stress on the weight of a heavy metal vessel [1]. The results of this work show the effect of heat treatment Welding post weld over the strength of welded joints in heavy metal vessels level. Unusual consideration is paid to

the size of the base plate which should be determined by the post-weld heat treatment. The results obtained show that, despite the fact that the current code requirements favor the C-Mn metal. Completely converted to Nb-micro alloyed steel, heated by combining high temperatures.

T.A Lechtenber and J.R. Fousds (1984) examined the effect of pre-microstructure warming, hardness and strength of HT-9 weldments

[2]. Reduced pre-heating temperatures, which affect the cooling rate of the hot-rolled steel, result in an increase in rack power and lower temperatures compared to non-charging steel welding. SEM tests show a reduced dendrite that separates and reduces interdendritic separation with a faster cooling rate. It is clear that the dynamic features of interdendritic ferrite and morphology as well as the dendrite separation, both of which are blocked by the cooling rate, play an important role in the distinct functioning of the weld metal separation. The results suggest that a significant reduction in premature heat by a good welding test results in significant advantages of weld metal welding equipment.

JN Clark (1986) investigated the preparation of low-strength weld metal weld without pre-heating and post-weld thermal treatment

[3] Additional information about welding welding was provided and talked about with reference to increased welding reliability.

D.G. Crawford and T.N. The Dough Puncher (1991) tested the microstructure and strength of the low carbon steel weld

[4]. Experimental experimental information was completed, due to the presentation that small groups were important areas for the use of weak leave, and that the effective or regular increase in this separation was a factor in the gross microstructure included. Subsequent interactions between a small structure and the power provided by means of protection against the impact of a variety of bonds with different strengths, through their small structural effects.

O.M. Akselsen and O. Grong (1992) examined the prediction of Charpy V score cast iron for a definitive elasticity and the acicular ferrite content. The charts can, thus, fill in as a reason for legitimate choice of consumables for welded steel structures.

[5]. Developments in some cases are produced in relation to the strength of the weld metal microstructure and elasticity. The relationship between expectations and analysis has

shown that the best understanding is achieved through the use of limited attributes.

V.S.R. Murti, P.D. Srinivas, G.H.D. Banadeki and K.S. Raju (1993) studied the effect of thermal conductivity on HSLA steel metallurgical structures multi-pass MIG welding [6]. Here its welding by Auto MIG welding using a 309L terminal wire is tested. This results in higher temperatures, higher statement rates and deeper penetration. Cooling rates are higher compared to SMAW, where the slag cover delivers lower cooling rates for weld dabs. Therefore, the high temperature of Auto MIG welding causes air to float in the welding area, resulting in their pollution. In line with these lines the input temperature may vary by changing the voltage and the additional current setting, however this is incorrect. High voltages alter the dab geometry and compound area, which influences the resulting small formation, and which can similarly obscure the circular phase and cause dispersion.

Alberto Sánchez Osio, Stephen Liu and David L. Olson (1996) examined the impact of cement on the development and development of carbon steel emission considerations [7]. Since compounds are nucleants in the proeutectoid phases, the proximity of these second-phase particles facilitates the transition to continuous cooling (CCT) into shorter periods. In this way, exposure to the construction and development of composite attracts previews of weld metal microstructure and structures. In their experiments, they proposed another model, considering a strong redistribution in the middle. An interesting feature of this model is that it predicts curve adjustment in order to spread the size with a mixed creation and a limited stiffness.

C.Smith, P.G.H. Pistorius and J. Wannenburg (1997) investigated the effect of heat treatment on post-burn therapy on the reliability of the welded member in a heavy metal container [8]. Multipass submerged-curve weld shafts are made by providing $1 \cdot 2$ and $4 \cdot 3$ kJ mm⁻¹ heaters. Isolation of microstructural areas identified in the warm climate of the actual weld was repeated. These areas were weak in the restored state. Warm treatment of post heat at 40 h at 620 °C brings about a significant improvement in Charpy's ability to touch. The explosive power of 134 kJ m² is estimated at the affected temperature range of $4 \cdot 3$ kJ mm⁻¹ after the thermal treatment delay after heating. The development of thermal energy through heat treatment of the post weld was noted by the melting of the structure.

N.Orhan, M Aksoy and N Orhan (1999) studied the effect of the horsepower ratio on the microstructure and structural properties of low-pressure and low-pressure (HAZ) machinery

[9]. In this experiment, the effects of coefficient of coarse grains and temperature fluctuations on a small building and mechanical properties of welding equipment and HAZ were studied. In welding tests, SAE 1020 steel models in hot tubs and grain swelling conditions were used. Following welding, microstructure structure, strength and durability of welding metals and HAZs were examined. From the results, a link has been established between the grain rating of the welding presentation and the suspended HAZ. The excess power of the HAZ of the limited grain starting model is achieved with high accuracy, while the maximum strength of the unique model is obtained by combining the average temperature.

S. H. Lalam, and H.K.D.H Badeshia et al. (2000) spread the test information by 2.25 trend Cr-1Mo will detect irritability [10]. Bruscato factor (X) is determined $(10P + 5Sb + 4Sn + As) / 100$ (at ppm). It has been found that phosphorus, silicon and manganese all make 2.25 Cr-1Mo stronger in anger, and reduced energy is reduced to that. Molybdenum reduces the tendency to pollute the initiated influence. Studies have also shown that there is no significant effect of arsenic, tin and antimony due to the potent effect of phosphorus.

J.C.F Jorge, L.F.G Souza and J.M.A Rebello (2001) examined the effect of chromium on microstructure / energy interactions in C– Mn weld metal stores.

[11]. The variety of chromium content is obtained by the extension of the various steps of the chromium powder in the welding channel. The interaction between the microstructure and power of the welding stores was focused on power paths, Charpy-V points and metallographic tests on cut models in contrast to weld dabs. The study of the subjects and the quantity of microstructural elements and the precision stages were performed with visual acuity and electron microscopy for filtration, each. The results showed that chromium weakens energy, despite promoting increased levels of acicular ferrite (AF). In addition, it has been noted that the increase in carbon content has significantly reduced the effect of congestion due to the complex volume of the M / A component.

M.A. Islam et al. (2003) studied the effect of previous estimates of austenite grains. Phosphorus was found to be an important trace element that can be separated from previous austenite grains.

[12]. This paper examined the separation of P during the opposite illumination (96 hours at 520 ° C) of 2.25Cr-1Mo fully dispersed and fully heated by Auger electron spectroscopy and demonstrates the isolation process. This paper also demonstrates the effect of P isolation in resisting cracking and cracking of non-explosive metals, one by one, by cracking at temperatures - 196 ° C to 20 ° C and fractography on the lens magnification lens. electron. This disintegration has led to a decrease in the rate of cracking of cooler and cooler metals at all test temperatures and a continuous increase in temperature. The micromechanism of the break in temperatures from the upper rack, in any case, remained unchanged.

V. Muthupandi et al. (2003) studied the impact of the science of welding metal and the impact of heat on the structure and properties of duplex treated steel welding.

[13]. The strong combination of solidarity and erosion of solid metals (DSS) is due to their strong organizational control and basic level balance. To achieve the proper balance of ferrite- austenite and structures, or a piece of welded metal and thermal insulation is controlled. The results found that (I) the composition of the mixture had a more significant effect on the ferrite- austenite component than the cooling rate, and (ii) even EBW which is considered a children's process in heating DSS, can be used in the filling methods provided. . increase can be observed.

Amit Kumar, MK Khurana and Pradeep K. Yadav (2016) This study provides the use of the Taguchi method combined with the gray relationship analysis to improve the parameters of the gas metal arc welding (GMAW) process of AISI 1020 carbon steels for additional quality . characteristics (bead width, bead length, weld penetration and affected temperature)

[14]. The orthogonal list of L9 is used to make members. The test is performed according to the combination of voltage (V), current (A) and welding speed (Ws). The results reveal that the welding speed is the most important process parameter. By analyzing related gray marks, correct parameters are obtained and key features are obtained using ANOVA analysis. Welding parameters such as speed, welding current and voltage are set to AISI 1020 material using the GMAW process. In order to ensure the validity of the test design, validation tests are performed on the parameter setting of the selected process. Viewing in this way may be helpful to sub-assemblies of vehicles, shipbuilders, shipbuilders, and pilots in order to obtain the right welding conditions. This paper deals with the use of Taguchi-related analysis in Gray to improve the welding

parameters of a gas metal arc. The multi-response development process uses an orthogonal system to perform tests in the form of GR and Taguchi. Properly setting the welding parameters reduces the bead width, HAZ bead length and increases welding penetration. It has been proven that most gas metal arc welding reactions are done in the form of a gray Taguchi. It was found that the percentage contribution to welding speed, voltage, and welding current was 90.08%, 4.55% and 0.66% respectively in weld bead geometry. The error also affects 4.68% which is mainly due to machine vibration and human error. GR-based welding parameters are 27 V power, 180 A current and welding speed of 52 cm / min.

Lenin Singaravelu D, Rajamurugan (2018) It is known that the greatest limitation of the traditional arc welding (GMAW) of various metals and stainless steel is the lack of a bridge and the production of a large amount of spatter. To overcome this difficulty, in recent years, waveform technology has been developed in the GMAW system to process specific applications to meet the required quality and production.

[15]. However, the specific advantage of various welding installation processes depends largely on the waveform parameters such as high current, background current, time and voltage. It is often found that improper waveform control leads to problems such as porosity, undercut and burn through etc. which interferes with the quality of the weld joint. Therefore, it is very important to study the effect of different waveform on bead geometry and microstructure. In this regard, current research aims to create different wavelengths in the heating of carbon and alloy steels.

Bead look, feel, analysis of large and small structure is done. Based on the results a very good waveform was obtained

2) During welding, in general, the V-I features of the short-range GMAW arc processor show that current and arc voltage have been found to increase with increasing power regardless of the base variation. 3) The level of weld joint produced by the modified process of short arc GMAW was improved with respect to the smooth appearance of weld bead geometry and the production of smaller spatter compared to conventional GMAW processes.

References:-

1. Makino, H. Evaluating methods of the propagating shear fracture in natural gas pipeline (Lecture for practical engineer) . Journal of the Japan Welding Society. 2007, vol. 76. no. 2, p. 114–117.

2. Hamada, M. Control of strength and toughness at the heat affected zone. *Journal of the Japan Welding Society*. 2002, vol. 71, no. 7, p. 22–26.
3. Ishigami, A. et al. Development of heavy wall high-strength UOE linepipe by means of microstructural control in base metal and seam weld. Proc. OMAE. paper OMAE-2011-50312.
4. Hirata, K. Physics of welding [III]. Melting rate and temperature distribution of electrode wire. *Journal of the Japan Welding Society*. 1994, vol. 63, no. 7, p. 484–488.
5. [6]International Energy Agency. Natural Gas Information. 2017.
6. International Energy Agency. CO2 Emissions from Fuel Combustion. 2016.
7. Ministry of Economy, Trade and Industry in Japan. “Sekiyu, tennengasu wo meguru saikin no doukou.” 2017.
8. J. R. Davis, “Alloying: Understanding the Basics”, Materials Park, OH, ASM International, 2001, pp. 193-209.
9. S.Benyounis, K.Y Olabi, Microstructural variations in a highstrength structural steel weld under isoheat input conditions of Weld. (November) 248-S–239-2008).
10. M. Menaka, M.Vasudevan, B.Venkatraman, B. Raj: NonDestructive Testing and Condition Monitoring, V.47, N. 9, pp 94- 98, 2005.
11. D.L. Olson, Effects of welding flux additions on 4340 steel weld metal composition, *Welding J.* (3) (1990) 115–122.
12. Ryabtsev, the removal of the slag skin and reduced the quality and productivity of surfacing, E.O. Paton Electric Welding Institute, Kiev, Russia 2008.
13. SUI Shao-hua , CAI Wei-wei, LIU Zhi-qiang, SONG Tian-ge, ZHANG, *JOURNAL OF IRON AND STEEL RESEARCH, INTERNATIONAL*. 2006, 13(2) : 65-68
14. Jerzy Nowacki, Paweł Rybicki, *Journal of Materials Processing Technology* 164–165 (2005) 1082–1088
15. C. S. Lee , R. S. Chandel & H. P. Seow *Materials and Manufacturing Processes*, VoL 15, No.5, 649-666, 2000
16. E L Makarov , H Herold , M Schtraitenberg & A Pshennikov *Welding International* 2009 14 (4) 305-309
17. Tomasz Kozak *Welding International*, 2015 Vol. 29, No. 8, 614– 618
18. Liangyun Lan n, Chunlin Qiu, DewenZhao, XiuhuaGao, LinxiuD, P.L. Harrison, R.A. Farrar, *Int. Mater. Rev*34 (1989) 35–51
19. K. Poorhaydari, B.M. Patchett, D.G. Ivey, *Mater. Sci. Eng. A* 430–436 (2006) 371–382].
20. C.L. Davis, J.E. King, *Metall. Mater. Trans. A* 25A (1994) 563– 573].
21. Cho, D.W., Na, S.J., Cho, M.H., Lee, J.S. 2013a. Simulations of weld pool dynamics in V-groove GTA and GMA welding. *Welding in the World* 57, 223–233.
22. Kanjilal, Majumdar, S.K Pal, T.K., Prediction of submerged arc weld-metal composition from flux ingredients with the help of statistical design of mixture experiment; *Scandinavian J. of Metallurgy*, V. 33, N. 3, 2004)
23. N. Murugan and V.Gunaraj. *Materials Processing Technology*, V.168, N.3, 2018.
24. M. Menaka, M.Vasudevan, B.Venkatraman, B. Raj: NonDestructive Testing and Condition Monitoring , V.47, N. 9, 2016
A. Daymi, M. Boujelbene, S. Ben Salem, B. HadjSassi, S. Torbaty “Effect of the cutting speed onthe chip morphology and the cutting forces” *Laboratory of handibio-esp, Team Mechanics Materials& High Speed Machining, University of the South Toulon-Var France , Volume 1, Issue 2 Dec 2009,Pages 77-83.*