

DYNAMIC ANALYSIS OF HONEY COMB STRUCTURE

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ABSTRACT

A honeycomb structure is a geometric arrangement of hexagonal cells, similar to the pattern found in a beehive. In engineering and materials science, honeycomb structures are typically composed of lightweight materials arranged in a hexagonal grid, creating a rigid and strong structure with minimal material usage. These structures are known for their high strength-to-weight ratio, making them advantageous in various applications. Materials like aluminum, composites, and even paper can be shaped into honeycomb structures. The design mimics the efficiency seen in natural honeybee hives, where hexagonal cells provide strength and stability with minimal use of resources.

In this, we are analysing the perforation of composite sandwich structures under high-velocity impact. We are using a three-dimensional finite element model modelled in Creo and implementing in Ansys to simulate sandwich panels with carbon/epoxy skins and an aluminium honeycomb core. We are evaluating the impact of individual components on the behaviour of the sandwich panel and determining the contribution of various failure mechanisms to the absorption of projectile kinetic energy. This project aims to provide insights into the present and future prospects of composite sandwich structures subjected to high-velocity impact.

INTRODUCTION

1.1 ABOUT HONEYCOMB STRUCTURE

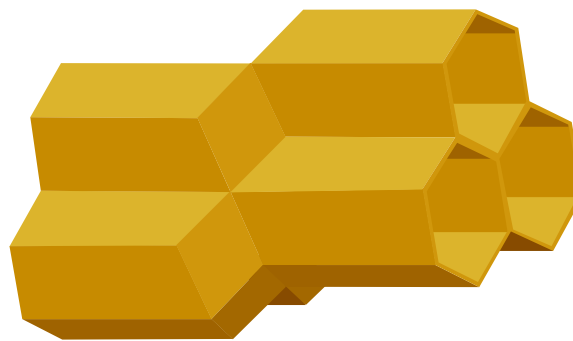


Figure no.1.1.1: Honeycomb structure

Honeycomb structures are natural or man-made structures that have the geometry of a honeycomb to allow the minimization of the amount of used material to reach minimal weight and minimal material cost. The geometry of honeycomb structures can vary widely but the common feature of all such structures is an array of hollow cells formed between thin vertical walls. The cells are often columnar and hexagonal in shape. A honeycomb-shaped structure provides a material with minimal density and relative high out-of-plane compression properties and out-of-plane shear properties.

Man-made honeycomb structural materials are commonly made by layering a honeycomb material between two thin layers that provide strength in tension. This forms a plate-like assembly. Honeycomb materials are widely used where flat or slightly curved surfaces are needed and their high specific strength is valuable. They are widely used in the aerospace industry for this reason, and honeycomb materials in aluminum, fiberglass and advanced composite materials have been featured in aircraft and rockets since the 1950s. They can also be found in

many other fields, from packaging materials in the form of paper-based honeycomb cardboard, to sporting goods like skis and snowboards.

LITERATURE REVIEW

- 1 **Akhil Garg:** An experimental study was conducted to investigate the impact of design parameters (wall thickness and cell size) on the mechanical properties, specifically yield strength and modulus of elasticity (stiffness), of honeycomb cellular structures produced through fused deposition modelling (FDM). Additionally, three computational intelligence (CI) based numerical modelling methods—genetic programming (GP), automated neural network search (ANS), and response surface regression (RSR)—were employed. The performance of these models in predicting the mechanical properties was compared, with statistical analysis revealing that the ANS model exhibited the highest performance, followed by GP and RSR models. The validity of the experimental findings was confirmed through 2D and 3D surface analyses conducted on models formulated using ANS.
- 2 **Enrique Barbero:** This study focused on analysing the perforation of composite sandwich structures when subjected to high-velocity impact. The sandwich panels under investigation featured carbon/epoxy skins and an aluminium honeycomb core. The analysis was carried out using a three-dimensional finite element model implemented in ABAQUS/Explicit. The model's accuracy was verified through experimental tests, where numerical results were compared with experimental data for residual velocity, ballistic limit, and contact time. The primary objective of the model was to assess the impact of individual components on the behaviour of the sandwich panel when exposed to impact loads. Furthermore, the study aimed to determine the contribution of various failure mechanisms to the energy absorption of the projectile's kinetic energy within the sandwich structure.
- 3 **B. CASTANIE:** In the aeronautical field, sandwich structures, commonly used for secondary components like flaps or landing gear doors, face a significant challenge in modelling low-velocity/low-energy impacts, which can reduce structural strength by up to 50%. As these impacts have a similar effect to quasi-static indentation, the study primarily focuses on understanding the behaviour of honeycomb cores under compression. To unravel the crushing mechanism, various honeycomb test specimens made of materials such as Nomex, aluminium alloy, and paper were examined. Observations during crushing, captured by a CCD camera, revealed rapid buckling of the cell walls. The peak load recorded during tests corresponded to the buckling of the common edge of three honeycomb cells. Additional tests on corner structures, simulating only one vertical edge of a honeycomb cell, exhibited a similar behaviour, with differences attributed to material properties. Based on this phenomenological study, it was hypothesized that the vertical edge primarily bears the loads during compression of a honeycomb core. Consequently, a simple analytical model using a grid of nonlinear springs was developed and validated through tests on Nomex™ honeycomb core indented by spherical indenters of different sizes. The analytical model demonstrated good correlation with experimental results, providing a basis for effectively modelling the indentation on a sandwich structure with a metallic or composite skin and honeycomb core using finite element analysis.
- 4 **Boudjemai:** This paper explores honeycomb panels used in the structural design of satellites, focusing on clamped-free boundary conditions. The study involves creating and analysing detailed finite element models for honeycomb panels. Experimental tests were conducted on a honeycomb specimen to compare modal analysis results obtained through finite element methods and existing equivalent approaches. The results indicate a strong agreement between finite element analysis, equivalent approaches, and experimental tests. The differences in the first two frequencies are less than 4%, and less than 10% for the third frequency. The equivalent model used in the analysis provides accurate results. The research also investigates various aspects of honeycomb plate modal analysis, including the impact of structural geometric variation and the influence of dimension parameters on modal frequency. Additionally, the study explores how changes in the core and skin materials of the honeycomb affect modal frequency. The results suggest that geometry parameters and material types indeed affect the honeycomb plate's modal frequency, providing promising insights.

METHODOLOGY

CREOPARAMETRIC

Step-11: Give Depth as 20mm in Symmetric.

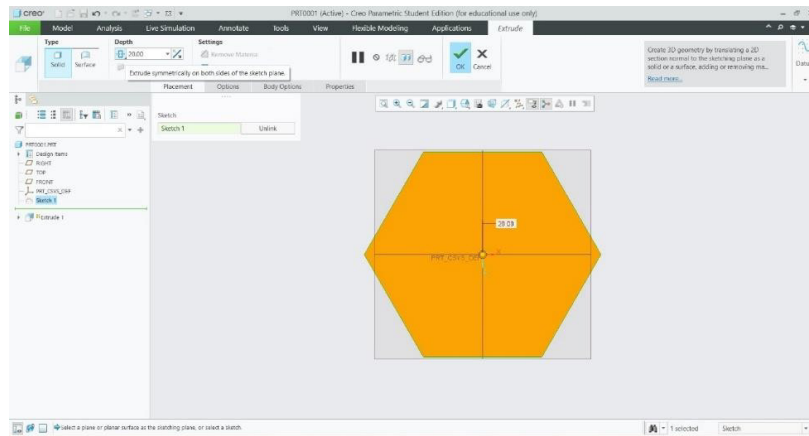


Figure no. 4.1.11: Extrude command selection

Step-13: Click on OK.

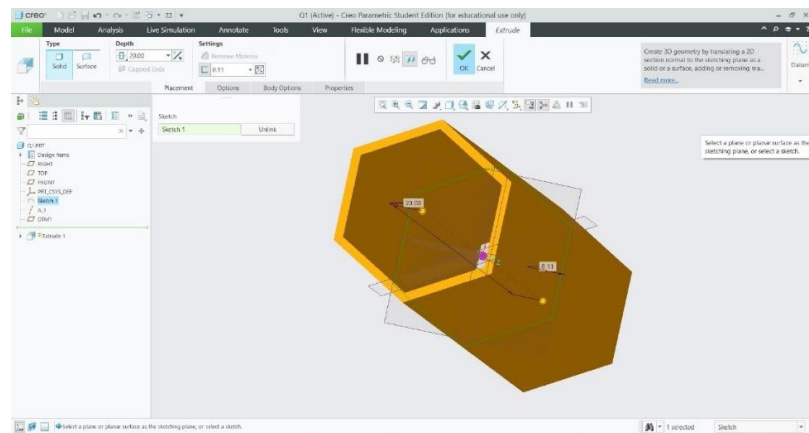
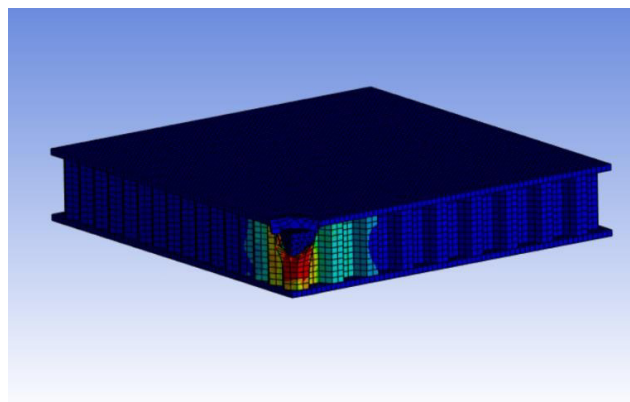


Figure no. 4.1.13: click on ok

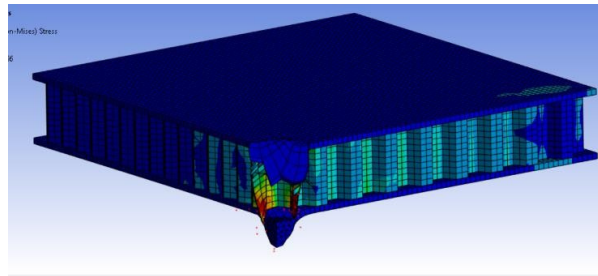
RESULTS

6.1 Evaluation of time from fiber failure criterion.



Figureno6.1.1:Fiberfailurecriterionatopplate.

- Heightofplate1(h1)=2mm =0.002m
- Velocityofball @h1 (v1)=362.11
- Time1 @h1(t1)= $\frac{h1}{v1} = \frac{0.002}{362.11} = 5.5 \times 10^{-6} \text{ s} = 5.5 \mu\text{s}$



Figureno.6.1.2:Fiberfailurecriterionatbottom plate

- Heightofsandwichstructure(h2)=24mm=0.024m
- Velocityofball @h2(v2)=363
- Time2 @h2(t2)= $\frac{h2}{v2} = \frac{0.024}{363} = 6.6 \times 10^{-5} \text{ s} = 66.1 \mu\text{s}$

Tableno6.1.1: Obtainedtimefrom fiberfailurecriterion

S.no	Time	Obtainedtime
1	T ₁	5.5 μs
2	T ₂	66.1 μs

Evaluating results from plastic strain during the sandwich perforation

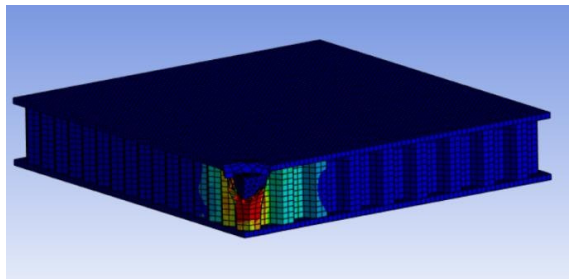


Figure no 6.2.1: Plastic strain at top plate.

- Height of plate 1 (h_1) = 2 mm = 0.002 m
- Velocity of ball @ h_1 (v_1) = 363.11 m/s
- Time 1 @ h_1 (t_1) = $\frac{h_1}{v_1} = \frac{0.002}{363.11} = 5.5 \times 10^{-6} \text{ s} = 5.5 \mu\text{s}$

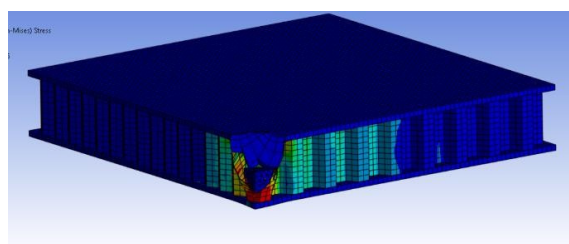


Figure no 6.2.2: Plastic strain at honeycomb structure.

- Height of honeycomb structure (h_2) = 24 mm = 0.024 m
- Velocity of ball @ h_2 (v_2) = 363 m/s
- Time 2 @ h_2 (t_2) = $\frac{h_2}{v_2} = \frac{0.024}{363} = 3.3 \times 10^{-5} \text{ s} = 33 \mu\text{s}$

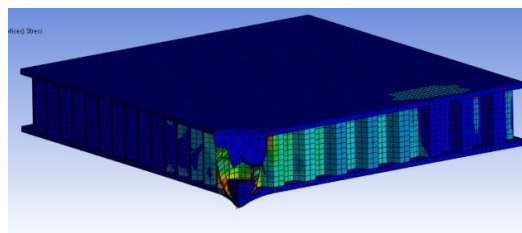


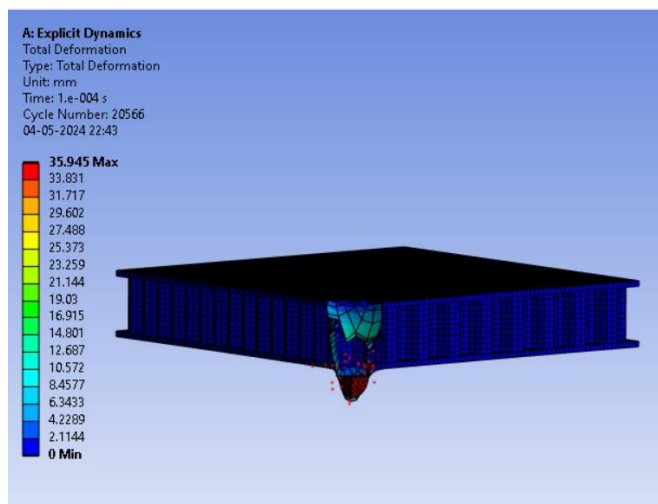
Figure no 6.2.3: Plastic strain at bottom plate.

- Height of the plate 2 (h_3) = 2 mm = 0.002 m
- Velocity of ball @ h_3 (v_3) = 363 m/s
- Time 3 @ h_3 (t_3) = $\frac{h_3}{v_3} = \frac{0.002}{363} = 6.6 \times 10^{-6} \text{ s} = 66 \mu\text{s}$

Table no 6.2.1: Obtained time from plastic strain criterion

S.no	Time	Obtained time
1.	T_1	5.5 μs
2.	T_2	33 μs
3.	T_3	66 μs

6.2 Totaldeformation



Figureno.6.3.1:Total deformation

Tableno.6.3.1:Total deformationvalues

S.No	Totaldeformationval ues (mm)	Color band
1	0	
2	2.1144	
3	4.2289	
4	6.3433	
5	8.4577	
6	10.572	
7	12.687	
8	14.801	
9	16.915	
10	19.03	
11	21.144	
12	23.259	
13	25.373	
14	27.488	
15	29.602	
16	31.717	
17	33.831	
18	35.945	

Equivalent stress

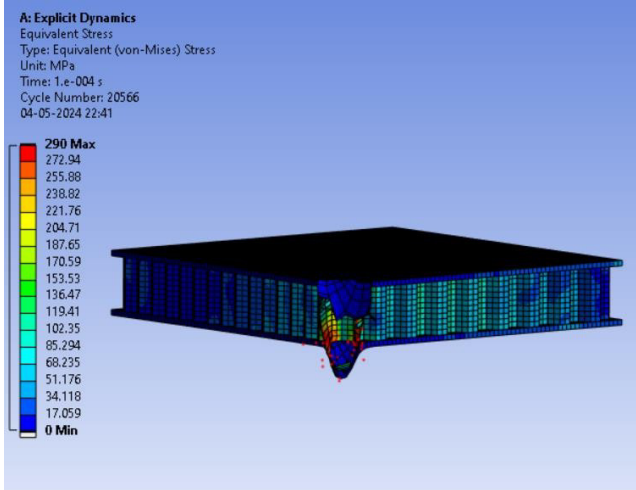


Figure no. 6.4.1: Equivalent stress

6.3 Equivalent Elastic strain

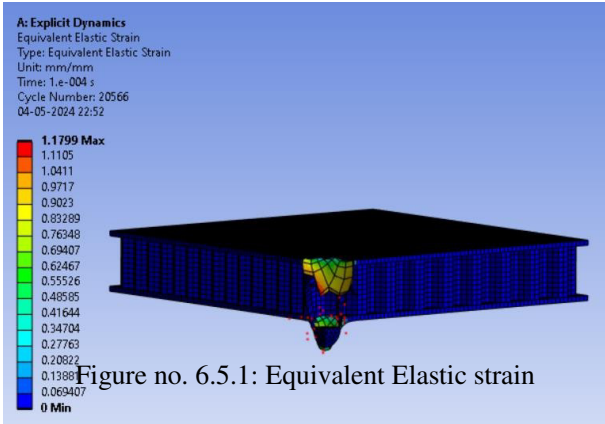


Figure no. 6.5.1: Equivalent Elastic strain

6.4 Total velocity

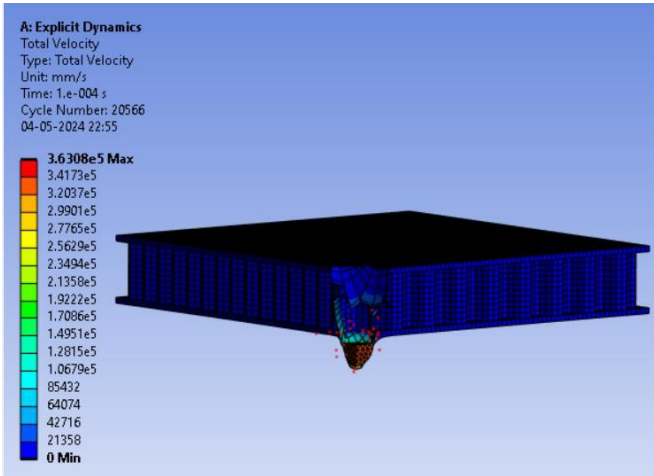


Figure no. 6.6.1: Total velocity

VALIDATION OF RESULT

7.1 Fiber-failure criterion during the sandwich perforation

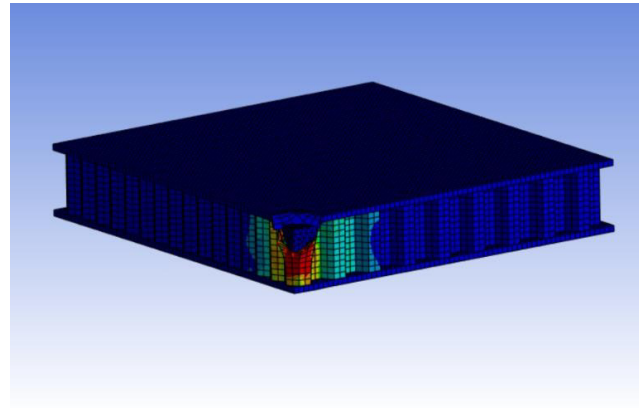
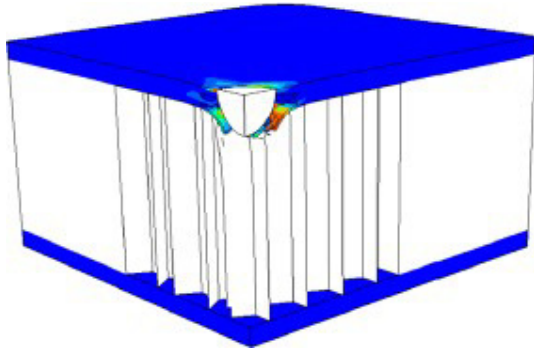


Figure no.7.1.1.1:Fiber failure creation top plate

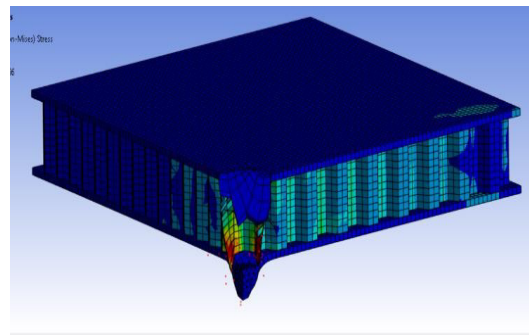
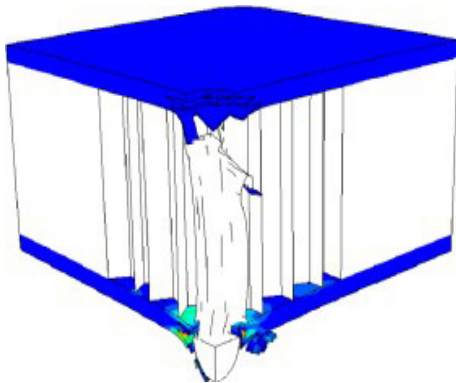
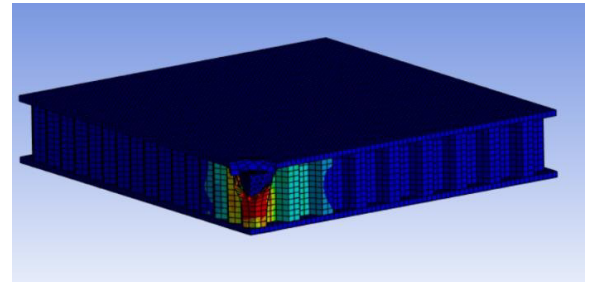
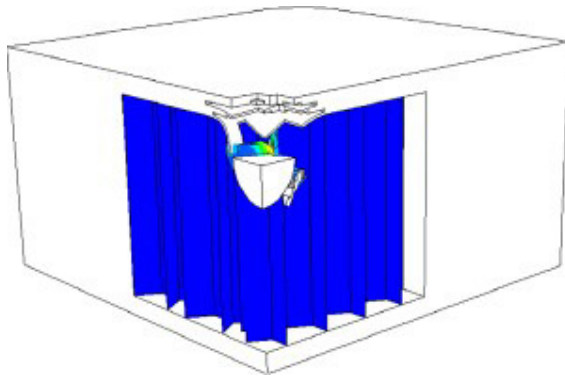


Figure no.7.1.1.2:Fiber failure creation bottom plate

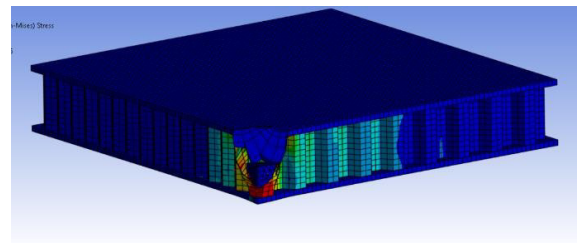
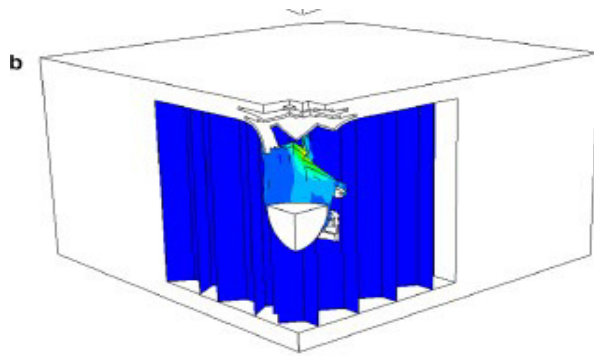
Table no.7.1.1: comparison between obtained and journal values during fiber failure.

Time	Reference Values	Obtained values
T1	7.2 μ s	5.5 μ s
T2	78.5 μ s	66.1 μ s

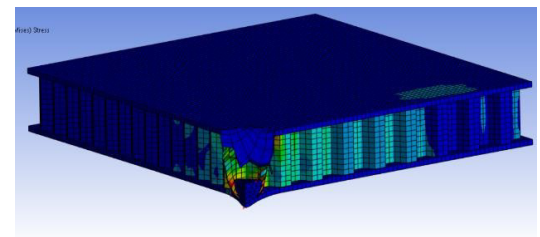
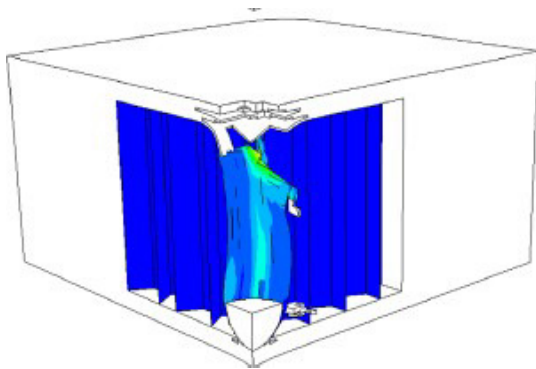
Evaluation of results from plastic strain during sandwich perforation



Figureno. 7.2.1: Plastic strain at top plate



Figureno.7.2.2: Plastic strain at honeycomb structure

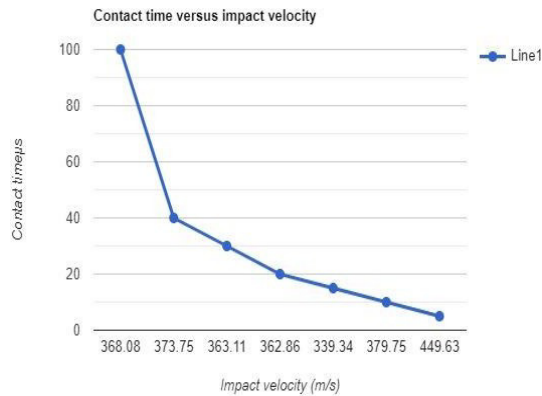


Figureno.7.2.3: Plastic strain at bottom plate

Tableno.7.2.1: Comparisonbetweenobtainedandjournalvaluesduringplasticstrain

Time	Referencevalues	Obtainedvalues
T1	7.2	5.5
T2	41	33
T3	78.5	66.1

7.2 ComparisonbetweenContacttimevsImpactvelocity



Figureno.7.3.1Contacttimevsimpact velocity

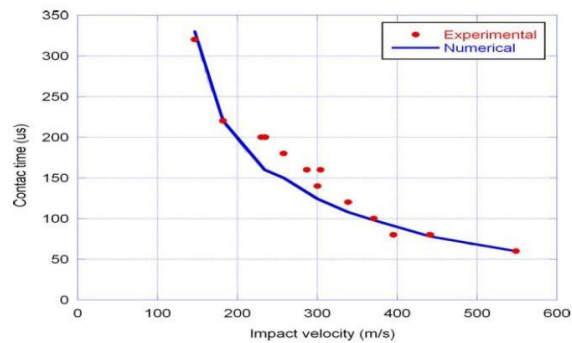


Fig. 4. Contact time versus impact velocity.

CONCLUSION

In this study the perforation of composite sandwich panel honeycomb structures subjected to high-velocity impact was analyzed using a three-dimensional finite element model implemented in ANSYS. Impact test was carried out to validate the journal model. Good agreement was found between journal results and experimental results.

The influence of both plates and core in the energy-absorption capabilities of the honeycomb sandwich panel was studied in a broad range of impact velocities. Most of the impact energy was absorbed by plates. For impact velocities 339 m/s, the impact energy was absorbed by the top plate and bottom plate. On the contrary the honeycomb core absorbed impact energy by plastic strain, at all the impact velocities analyzed. Also, the energy-absorption mechanisms in both plates and the core were studied. The main mechanism in the plate was fiber breakage whereas in the core the mechanism was the plastic deformation of the aluminum core. Both in the plates and the core, the damage was concentrated in a small area around the impact point.

8.1 FUTURE PROSPECTS

While our study provides valuable insights, further research is warranted to explore advanced materials, innovative manufacturing techniques, and multi-scale modeling approaches for predicting ballistic performance. Additionally, investigating the long-term durability and environmental sustainability of honeycomb-based composite materials is crucial for their widespread adoption.

Our findings underscore the efficiency of honeycomb structures as composite materials, offering superior protection against high-velocity projectiles. By advancing our understanding of their behavior and optimizing their design, we can enhance the safety

y and security of individuals in high-risk environments. Sustainability of honeycomb-based ballistic materials is crucial for their widespread adoption.

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